

## Microstructure and High Temperature Oxidation Behavior of **ZrB<sub>2</sub>-ZrO<sub>2</sub>-MoSi<sub>2</sub>-Al Coatings for the Protection of Carbon/Carbon Composites** <u>VY. Novikov<sup>1</sup>, M.G. Kovaleva<sup>1</sup>, IY. Goncharov<sup>1</sup>, M.N. Yapryntsev<sup>1</sup>, Y.N. Tyurin<sup>2</sup>, VY. Sirota<sup>3</sup>, O.N. Vagina<sup>1</sup>, I.N. Pavlenko<sup>1</sup>, O.V. Kolisnichenko<sup>2</sup> <sup>1</sup>Belgorod State National Research University, Belgorod, 308015, RU.</u>

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The  $ZrB_2$ - $ZrO_2$ -MoSi\_2-Al composite coatings were prepared on the carbon/carbon composite using a new multi-chamber detonation accelerator by thermal spraying methods from micro-powders. The initial powders  $ZrB_2$ -xMoSi<sub>2</sub> (x = 24, 35, 45 wt %) with 5 wt %  $Y_2O_3$  and 20 wt % Al.  $Y_2O_3$  were successfully used as a stabilizer of the high temperature tetragonal and cubic modification of zirconia. Aluminum was added as an oxidizing agent during spraying and creating "plastic" lamellae and nano-dispersed inclusions, relieve internal stresses. In the present work, the microstructure, elemental and phase composition of coating were investigated by scanning electron microscopy (SEM) and X-ray diffraction (XRD) before and after annealing at 1500°C in air for 1 h.



White phase (globular grains) consists of  $ZrO_2$ , the light gray phase is mullite  $(3Al_2O_3 \cdot 2SiO_2)$ , amorphous  $SiO_2$ and  $Al_2O_3$  with a hexagonal crystal lattice.

**Figure 1.** SEM-BSE micrograph (a) and XRD diffraction pattern (b) of the composite powder ZrB<sub>2</sub>-MoSi<sub>2</sub>-Al.

MCDS multi-chamber detonation accelerator





**Figure 2.** Cross-section SEM-BSE micrographs of the ZrB<sub>2</sub>– MoSi<sub>2</sub>-Al coating: general view (a), high magnification (b), coating–substrate interface (c), and XRD diffraction pattern.

		Phase composition, %				
Coating	c-ZrO <sub>2</sub>	o-Al <sub>4.64</sub> Si <sub>1.36</sub> O <sub>9.69</sub>	m-ZrO <sub>2</sub>	h-Al <sub>2</sub> O <sub>3</sub>	t-ZrO	
a Zr24MoY/2	DAI 35	47	5	13	-	
b Zr35MoY/2	DAI 35	57	6	2	_	
c Zr45MoY/2	DAI 5	62	3	-	30	
Figure 3.	XRD patterns,	, SEM-BSE micro	ographs a	and phas	se	

temperature oxidation.

## high-temperature oxidation 1500 °C

>Uniform dense coatings with good adhesion to the substrate were obtained, the bulk of the coating material was deformed and tightly packed, but the presence of unmelted zirconium particles in the coatings was observed. The porosity of the composite coatings was 0.02-1.00%.

>The visible boundary of the adhesion of the composite coatings to the C/C substrate has no defects. In the contact zone of the coatings and the substrate, a mixed structure is observed, consisting of coating islands in the substrate with different shape and size. Some of the powder material has penetrated deeply and is firmly bonded to the substrate material.

> Composite coatings consist of tetragonal and monoclinic ZrO<sub>2</sub>, hexagonal ZrB<sub>2</sub>, fcc-Al, tetragonal MoSi<sub>2</sub>.

> It was found that an increase in the content of MoSi<sub>2</sub> in the initial powder mixture during high-temperature oxidation of the coating formed from it leads to an increase in the content of mullite ( $3Al_2O_3 \cdot 2SiO_2$ ), which is formed in the form of the finest intertwined needle-shaped crystals.

> It was shown that an increase in the MoSi<sub>2</sub> content in the initial powder mixture during high-temperature oxidation of the coating formed from it leads to one-sided diffusion of SiO<sub>2</sub> into the Al<sub>2</sub>O<sub>3</sub> grain with the formation of mullite. In place of the initial glass phase SiO<sub>2</sub>, pores are formed.

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